

## **S-Parameter Analysis of Parallel Coupled Line Bandpass Filter With Comsol Multiphysics**

**Mun Hoe Teh<sup>1</sup>, Rosmila Abdul-Kahar<sup>1\*</sup>, Nurafiqah Mohd-Alhata<sup>1</sup>, Mohamad Mazlan Rozali<sup>1</sup>**

<sup>1</sup> Photonics Devices and Sensor Research Center (PDSR)  
Department of Physics and Chemistry  
Faculty of Applied Sciences and Technology  
Universiti Tun Hussein Onn Malaysia  
84600 Pagoh, Muar, Johor, MALAYSIA

\*Corresponding Author Designation

DOI: <https://doi.org/10.30880/ekst.2023.03.01.004>

Received 02 January 2023; Accepted 21 January 2023; Available online 3 August 2023

**Abstract:** Nowadays as the global internet growing in high speed and the 5G flourish the demand of high-speed data transfer with low delay are still in progress. As 5G devices component, the microwave filters are functioned to transmit and to filter the signal (data) within the interest frequency range. Microwave filters are currently having problems such as insufficient of bandwidth due to the wide range of transmission signal frequency, large insertion loss. At the same time, parallel coupled line bandpass filters are being used for a wider range of frequency for passband and a more stable insertion loss, 5G parallel couple line bandpass filters with Patterned Ground Structure (PGS) technique using COMSOL Multiphysics software is designed and compared with reference filter (parallel coupled line bandpass filter). The effect of substrate size, strip/slot size and shape on S-parameter and electromagnetic field simulation results are presented and filter(s) design with better S-parameter is proposed. The small square strip medium substrate filter has 8.7% of improvement on the lowest  $S_{11}$  compared to reference filter, whereas the big O strip medium substrate has 20.3% and 8.7% of improvement for both maximum  $S_{11}$  and minimum  $S_{11}$  compared to the reference filter. The most preferable design filter is the small square strip with medium substrate having  $S_{21}$  -2 dB and  $S_{11}$  -20 dB.

**Keywords:** Microwave Filter, Coupled Line Bandpass Filter, Electromagnetic Field Simulation, S-Parameter

---

\*Corresponding author: [rosmila@uthm.edu.my](mailto:rosmila@uthm.edu.my)

## 1. Introduction

Nowadays as the global internet growing in high speed and the 5th generation (5G) flourish the demand of high-speed data transfer with low delay, related researches for improvement are just recently in progress [1]. So 5G technology is still a long way to be fully utilized in big data, industry and internet of things (IoT) [1].

Microwave filters or sometime called filters being one of the components of 5G devices such as smartphone, laptop, 5G internet modem being used for transmitting, filtering and receiving signals (data) of different frequency range. Filters can be classified into high pass, low pass, band pass and band stop filters [2]. Active filters will have at least 1 operational amplifier (op-amp), while passive filters have no op-amp within the circuit. The order of filters is based on the number of reactive components within the filter circuit, filters having 1 capacitor or inductor are called first order [3]. Parallel coupled bandpass filters and Patterned Ground Structure (PGS) technique are commonly used in filters for a wider frequency range for passband and stabler insertion loss,  $S_{21}$  and so high-speed 5G internet [4]. Filters are currently having problems such as insufficient of bandwidth due to the wide range of transmission signal frequency, large insertion loss  $S_{21}$  [5]. Filter property, scattering parameter also known as S-parameter represented by  $S_{21}$  and  $S_{11}$ , the ability of a filter to transfer electrical signal throughout the filter known as the signal absorption or insertion loss being denoted by  $S_{21}$  having negative magnitude, while the ability for a filter to reflect electrical signal by the filter known as the reflection loss is denoted by  $S_{11}$  also having negative magnitude.

Simulating filter circuit through software such as Multiphysics Simulation Software COMSOL, Computer Simulation Technology (CST), Advanced Design System (ADS), Genesys and others, with electromagnetic (EM) field simulation we able to maximize the number of trials without producing filters with undesirable features, reducing yield cost and waste [4].

The research aims including designing 5G parallel couple line bandpass filters with Patterned Ground Structure (PGS) technique using COMSOL Multiphysics software. The effect of substrate size, strip/slot size and shape on S-parameter and electromagnetic field simulation results is also studied. The filter(s) design with better  $S_{21}$  and  $S_{11}$  compared to the filter from [5] is fabricated.

## 2. Materials and Methods

COMSOL was used for the simulation due to its availability and ease for using. In this project Patterned Ground Structure (PGS) technique is used to better enable unwanted frequency rejection and improve the electrical performances [5].

### 2.1 Parameter

The filter specifications are shown as Table 1 where the operating frequency referring to the signals within a range of frequency having a significant low insertion loss  $S_{21}$  expected between 6-13 GHz these frequencies also categorized as C,X, Ku band of microwave that being used by 5G devices [6]. The electrical signals simulate the microwave mentioned in Table 1. The substrate referring to the base material used in COMSOL simulation as the major part of the filter [7], in this research all the filters substrate are using Rogers 4003C ( $\epsilon_r = 3.38$ , low loss) ; substrate thickness referring to the thickness of substrate, 0.5mm for small substrate, 0.508mm for medium substrate [5] and 1mm for big substrate; the strip referring to both microstrip (top patch) and metallic strip (ground patch), using perfect electric conductor; line impedance referring to the impedance matching [5], using 50  $\Omega$ ; return loss  $S_{11}$  referring to the loss of strength of returning or reflected signals, expected to be less than -30dB; insertion loss  $S_{21}$  referring to the loss of transmitting signals power, expected to be as 0 as possible.

**Table 1: Design specifications**

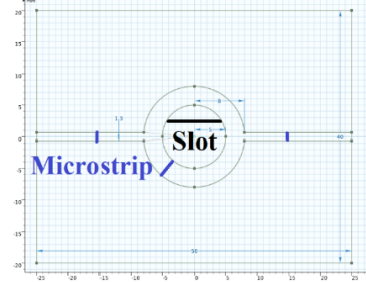
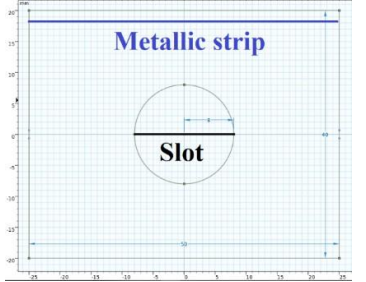
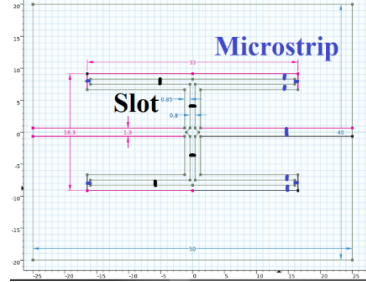
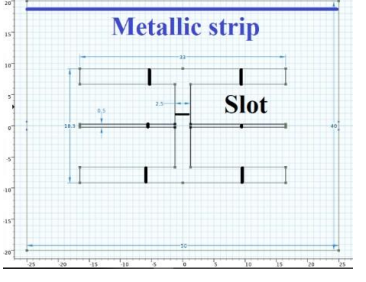
Specifications	Value
Operating Frequency	6-13 GHz [5]
Substrate	Rogers 4003C ( $\epsilon_r=3.38$ F/m)(low loss)
Substrate Thickness	0.5 mm, 0.508 mm, 1 mm
Strip	Perfect electric conductor
Line Impedance	50 $\Omega$
Reflection loss $S_{11}$	$\leq -30$ dB
Insertion loss $S_{21}$	0 dB

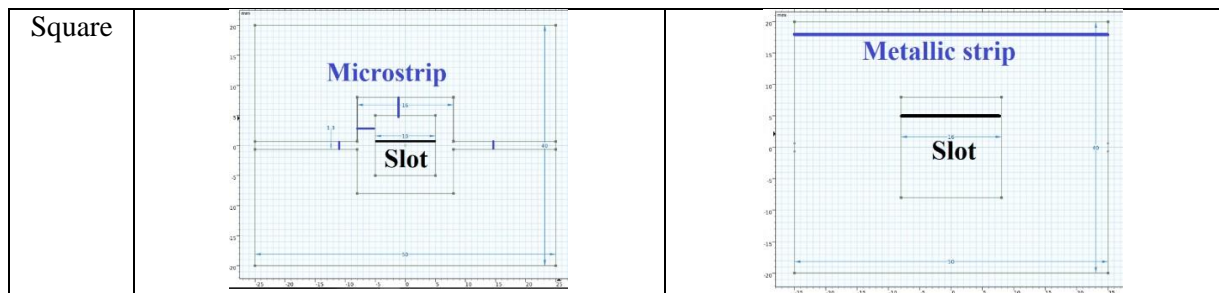
2.2 Geometry

There are 3 sizes of filter substrate which are called as the small size, medium size (reference substrate size) [5] and big size substrate, with dimensions; length x width x thickness as following: small substrate (40mm x 20mm x 0.5mm), medium substrate (46mm x 34mm x 0.508mm) [5] and big substrate (50mm x 40mm x 1mm).

Each substrate size filter has 3 different strip/slot shapes; circular (O), E and square shape. All shapes are further categorized into 2 sizes which are big and small shape; big/small O, big/small E and big/small square. Some design filters are shown in Table 2, while Table 3 shows all the design filters' dimensions.

**Table 2: Top and ground patch of some design filters**

Shape	Top patch	Ground patch
Circular (O)		
E		



**Table 3: Substrate size, strip/slot size and shape for all design filters**

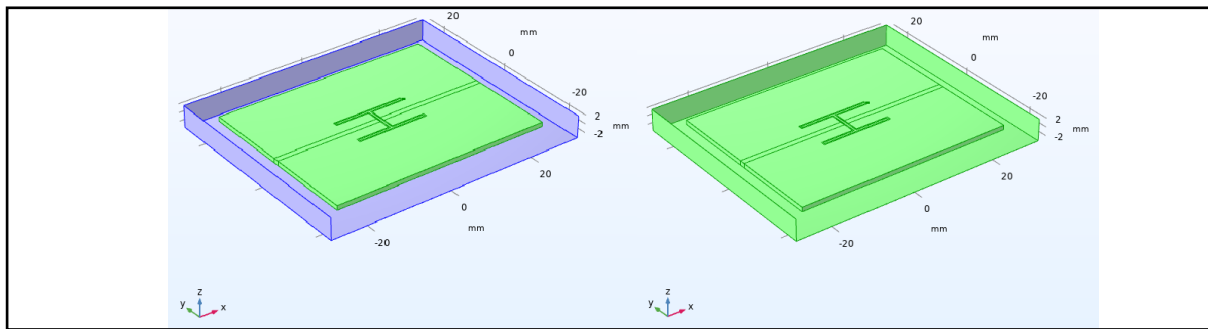
Substrate size (mm x mm x mm)	Shape of Strip / slot	Shape size	Top patch Microstrip size (mm)	Top patch slot size (mm)	Ground patch slot size (mm)
Small (40 x 20 x 0.5)	O (radius)	Small	1	3	4
	E		0.283	0.48	1.046
	Square (side)		1	6	8
	O (radius)	Big	3	5	8
	E		0.85	0.8	2.5
	Square (side)		3	10	16
Medium (46 x 34 x 0.508)	O (radius)	Small	1	3	4
	E		0.283	0.48	1.046
	Square (side)		1	6	8
	O (radius)	Big	3	5	8
	E		0.85	0.8	2.5
	Square (side)		3	10	16
Big (50 x 40 x 1)	O (radius)	Small	1	3	4
	E		0.283	0.48	1.046
	Square (side)		1	6	8
	O (radius)	Big	3	5	8
	E		0.85	0.8	2.5
	Square (side)		3	10	16

### 2.3 Patterned Ground Structure (PGS)

PGS also known as the Patterned Ground Structure technique is one of the techniques for improving the performance of microwave filter and also for enabling the unwanted frequency rejection of the signal [5]. The second column (ground patch) in Table 2 above shows the PGS for different shapes. Both metallic strip and the slot that located at the bottom part of the filter are considered as the PGS as they are contributing the electrical properties for the filter at the bottom patch [8].

### 2.4 Scattering boundary condition

Scattering boundary condition is to define the simulation boundary so that the EM field simulation will not run beyond the defined boundary at the same time allowing the scattering wave to pass through certain boundaries [4]. For this paper the scattering boundary condition was defined for all the domains including the surrounding and the design filter as shown as Figure 1. Whereas the scattering boundary condition is governed by the *Eq. 2*.



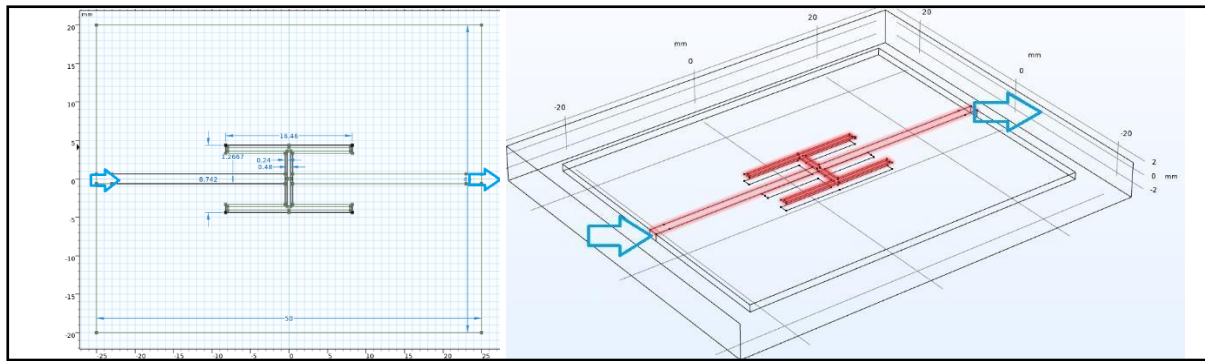
**Figure 1: Left figure is the scattering boundary condition of the filter domain. Right figure is the scattering boundary condition of the surrounding domain**

### 2.5 Meshing

Meshing also known as mesh generation representing one of the important steps in simulation that involve thousands or more of shapes for defining the physical shape of the filter [9]. A detail meshing is needed for a better accuracy of 3D CAD model [1]. After the meshing, the simulation will be run and filter property result such as S-parameter will be plotted based on the design of the filter.

### 2.6 Equations

The input electrical signal that passing through all of the design filters from input port shown by the blue arrow in Figure 2 is set constantly such that the voltage of input signal is 1 V and 50  $\Omega$  as reference impedance also known as characteristic impedance [10] with uniform port using cable at 0 port phase with the output signal. While the output electrical signal passing through all of the design filters out of the output port shown by blue arrow in Figure 2 is set constantly with uniform port made by cable with 1 V and 50  $\Omega$  reference impedance as well. *Eq. 1* below showing the formulae to obtain the impedance,  $Z$ . The current set to 0.02 A for both the input and output port.



**Figure 2: Left figure showing top view, right figure showing isometric view of an E strip filter with arrows indicating the direction of electric signal and the position of port 1 and port 2**

$$Z = \frac{2Z_{0e} Z_{0o} \sin \theta}{\sqrt{(Z_{0e} - Z_{0o})^2 - (Z_{0e} + Z_{0o})^2 \cos^2 \theta}} \quad \text{Eq. 1}$$

where,

- $Z$  = Matching impedance,  $\Omega$
- $Z_{0e}$  = Even mode impedance,  $\Omega$
- $Z_{0o}$  = Odd mode impedance,  $\Omega$
- $\theta$  = Signal phase

$$\nabla \cdot (\mu_r^{-1} \nabla E) - k_0^2 \epsilon_r E = 0 \quad \text{Eq. 2}$$

where,

- $E_z$  = Electric field at z-axis
- $\mu_r$  = Relative permeability, H/m (equal to 1 in vacuum)
- $\epsilon_r$  = Relative permittivity, F/m (equal to 1 in vacuum)
- $k_0$  = Wave number

The capacitance and inductance are also the important properties of filters and being shown as Eq. 3 for filter capacitance and Eq. 4 for filter inductance.

$$C_p = \frac{f_c}{4\pi Z_e} \left( \frac{1}{f_o^2 - f_c^2} \right) \quad \text{Eq. 3}$$

$$L_p = \left( \frac{1}{4\pi^2 f_o^2 C_p} \right) \quad \text{Eq. 4}$$

### 3. Results and Discussion

By analyzing the S-parameter, the performance of design filters and also the factors effecting the performance of filter can be determined.  $S_{21}$  and  $S_{11}$  are two important parameters of filters. Insertion loss,  $S_{21}$ , known as the signal loss while signal transmitted from port 1 to port 2, so it is necessary to be stable and as low as possible (as 0 as possible), the lower the  $S_{21}$ , indicate the lower loss of signal, the stabler the  $S_{21}$ , indicate the lower discontinuity of signal, its value is negative in the S-parameter in order for considering the signal loss during the transmission.

Reflection loss,  $S_{11}$ , known as the signal loss while being transmitted to port 1 from the signal generator and reflected at port 1, so it is necessary to be as much as possible, the bigger the negative value of  $S_{11}$ , indicate more signal loss during the reflection at port 1, that's mean more signal being transmitted to the network within the filter, its value is negative in the S-parameter in order for considering the signal loss during the reflection.

Table 4 referring to the S-parameter of design filters with small strip/slot arranged based on their substrate size and strip/slot shape to analyze the effect of substrate size and strip/slot shape toward the S-parameter. While Table 5 referring to the S-parameter of design filters with big strip/slot arranged based on their substrate size and strip/slot shape to analyze the effect of substrate size and strip/slot shape toward the S-parameter.

#### 3.1 S-parameter comparison with different substrate size

By observing the Table 4, for small strip filters, the filters with medium substrate (46mm x 34mm x 0.508mm) [5] have lower insertion loss  $S_{21}$  (less power loss during signal transmission) and higher reflection loss  $S_{11}$  (more signal able to be transmitted due to high reflection loss) compare to small and big substrate filters. Medium substrate filters (red words) have stabler  $S_{21}$  (Small O: -2dB, Small E: -3.5dB, Small square: -2dB) of insertion loss they also have larger average reflection loss  $S_{11}$  compare to small and big substrate filters (Small O: -15dB, Small E: -14dB, Small square: -20dB) meaning better performance (lower power loss for signal transmission and more signal able to be transmitted to the network within the filter due to high reflection loss) compare to other same strip/slot shape and size but different substrate size filters. When compare to reference filter that has  $S_{21}$  -1.76dB and average  $S_{11}$  -14.69dB [5], the small square is better for its  $S_{11}$  (-20dB) but not better in  $S_{21}$  (-2dB).

By observing Table 5, the filter with medium substrate (46mm x 34mm x 0.508mm) [5] having better filter performance compare to other substrate size filters in term of  $S_{21}$  and  $S_{11}$  except the big square strip filter with small substrate (Big square:  $S_{21}$  = -4.5dB and  $S_{11}$  = -14dB) (marked red star), they have relatively stable  $S_{21}$  (Big O: -4dB, Big E: -6dB) of insertion loss (less power loss during signal transmission) and larger average reflection loss  $S_{11}$  (more signal able to be transmitted due to high reflection loss). Medium substrate filters (red words) having larger average reflection loss  $S_{11}$  (Big O: -20dB, Big E: -15dB) meaning better performance (lower power loss for signal transmission and more signal able to be transmitted to the network within the filter due to high reflection loss) compare to other same strip/slot shape and size but different substrate size filters. When compare to reference filter that has  $S_{21}$  -1.76dB and average  $S_{11}$  -14.69dB [5], the big O is better for its  $S_{11}$  (-20dB) but not better in  $S_{21}$  (-4dB).

#### 3.2 S-parameter comparison with different strip/slot shape

In case of comparing the S-parameter of design filters by its strip/slot shape in Table 4 and Table 5. For small substrate and small strip filters, O strip filter (marked blue cross) has stabler  $S_{21}$  and almost 0dB and larger average  $S_{11}$  -16dB so it has lower power loss for signal transmission and more signal

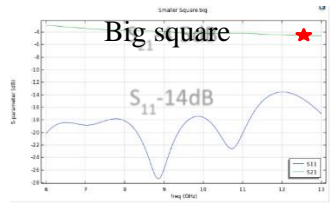
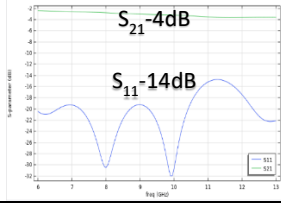
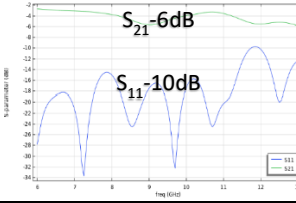
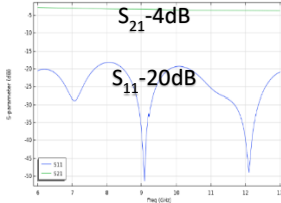
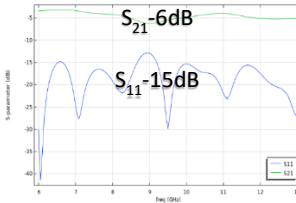
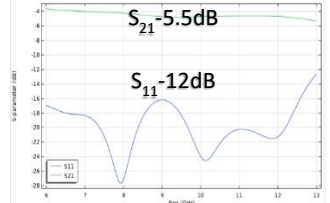
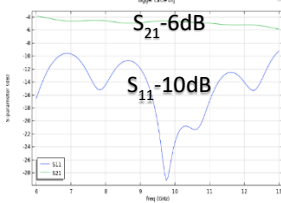
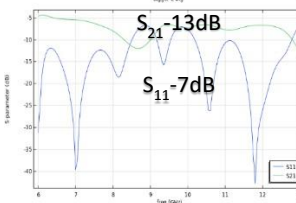
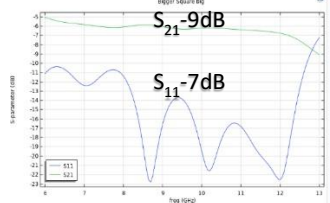
able to be transmitted to the network within the filter due to high reflection loss compare to small E and small square filters. For medium substrate and small strip filters, square strip filter (marked blue cross) has more stable  $S_{21}$  and almost 0dB and larger average  $S_{11}$  -15dB so it has lower power loss for signal transmission and more signal able to be transmitted to the network within the filter due to high reflection loss compare to small O and small E filters. For big substrate and small strip filters, O strip filter (marked blue cross) has more stable  $S_{21}$  and almost 0dB and larger average  $S_{11}$  -8dB so it has lower power loss for signal transmission and more signal able to be transmitted to the network within the filter due to high reflection loss compare to small E and small square filters. For all the big strip filters with any substrate size, O strip filters (red words) are always better than other big strip filters with more stable  $S_{21}$  and almost 0dB and larger average  $S_{11}$  (small substrate: -14dB, medium substrate: -17dB, big substrate: -10dB) so they have lower power loss for signal transmission and more signal able to be transmitted to the network within the filter due to high reflection loss compare to big E and big square filters.

**Table 4: S-parameter with different substrate size of small strip/slot shape**

		Strip/slot shape and size		
Substrate size (mm x mm x mm)		Small O	Small E	Small square
Small (40 x 20 x 0.5)	Small O	$S_{21}$ -2dB $S_{11}$ -16dB	Small E	$S_{21}$ -2.5dB $S_{11}$ -10dB
	Small E	$S_{21}$ -2dB $S_{11}$ -15dB	Small square	$S_{21}$ -2.5dB $S_{11}$ -15dB
	Small square	$S_{21}$ -3.5dB $S_{11}$ -14dB	Small O	$S_{21}$ -2dB $S_{11}$ -20dB
Medium (46 x 34 x 0.508)	Small O	$S_{21}$ -4dB $S_{11}$ -9dB	Small E	$S_{21}$ -6dB $S_{11}$ -4dB
	Small E	$S_{21}$ -4dB $S_{11}$ -6dB	Small square	$S_{21}$ -4dB $S_{11}$ -6dB
	Small square	$S_{21}$ -4dB $S_{11}$ -6dB	Small O	$S_{21}$ -4dB $S_{11}$ -6dB



**Table 5: S-parameter with different substrate size of big strip/slot shape**

		Strip/slot shape and size		
Substrate size (mm x mm x mm)	Big O	Big E	Big square	
				
Small (40 x 20 x 0.5)				$S_{21}$ -4.5dB $S_{11}$ -14dB
Medium (46 x 34 x 0.508)				
Big (50 x 40 x 1)				

#### 4. Conclusion

Based on the analysis, for Table 4, the best design filter among 9 filters in term of  $S_{21}$  and  $S_{11}$  is the small square strip with medium substrate has most stable and lowest  $S_{21}$  -2dB and largest average  $S_{11}$  between -16dB to -50dB. For Table 5, the best design filter among 9 filters in term of  $S_{21}$  and  $S_{11}$  is the big O strip with medium substrate has the most stable and lowest  $S_{21}$  -4dB and largest average  $S_{11}$  between -20dB to -50dB. While the reference filter has  $S_{21}$  -1.76dB and  $S_{11}$  -16.62 as low as -46dB [5]. The small square strip medium substrate filter has 8.7% of improvement on the lowest  $S_{11}$  compared to reference filter [5], whereas the big O strip medium substrate has 20.3% and 8.7% of improvement for both maximum  $S_{11}$  and minimum  $S_{11}$  compared to the reference filter [5]. In other words, for small strip/slot shape filters those filters with square shape and medium substrate size is better and for big strip/slot shape filters those filters with O shape and medium substrate size is better, but the prior filter is the best among all the 18 design filters.

#### Acknowledgement

This study was supported by the Ministry of Higher Education (MOHE) through Fundamental Research Grant Scheme (FRGS) (FRGS/1/2019/STG02/UTHM/02/1) and Universiti Tun Hussein Onn Malaysia (UTHM) through vote K173. The authors would also like to thank the Faculty of Applied Sciences and Technology, Universiti Tun Hussein Onn Malaysia for its support.

## References

- [1] N. N. Al-Areqi, N. Seman and T. A. Rahman, "Parallel-coupled line line bandpass filter using different substrate for fifth generation wireless communication applications," International Symposium on Antennas and Propagation, ISAP 2015, (C), pp.953-956.
- [2] P. Hazdra, M. Polivka and V. Sokol, "Microwave antennas and circuits modeling using electromagnetic field simulator," Journal of Radioengineering, vol. 14, no. 4, pp. 149-159, 2005.
- [3] Z. S. Kiss, A. M. Rostas, L. Heidinger, N. Spengler, M. V. Meissner, N. MacKinnon and G. J. Korvink, "A microwave resonator integrated on a polymer microfluidic chip," Journal of Magnetic Resonance, 2016, pp. 270.
- [4] R. O. Rourke, 3D Electromagnetic Simulation vs. Planar MoM. Microwave Journal, pp. 68 - 76. 2015.
- [5] U. H. Morshidi, D. N. Abang Zaidel, N. Seman, M. P. Attan, D. A. Awang Mat, M. R. Mohd Sharip and H. Kanaya, "Bandwidth Enhancement of 5G Parallel Coupled Line Band Pass Filter Using Patterned Ground Structure Technique," International Journal of Integrated Engineering, 12(6), pp.87-93.
- [6] J. U. Duncombe, "Microwave Navigation – Part II: An Assessment of Feasibility," IEEE Trans. Electron. Devices, vol. ED-14, pp. 40-50, Feb. 2005.
- [7] Infineon Technologies, "5G - The high-speed mobile network of the future - EE Times Asia. EET Asia," IEEE Microwave and Wireless Components Letter, 28(12), pp.1110-1112.
- [8] D. Psychogiou and R. Gomez-Garcia, "Reflectionless Adaptive RF Filters: Bandpass, Bandstop, and Cascade Designs," IEEE Transaction on Microwave Theory and Technique, 65(11), 2017, pp.4593-4605.
- [9] J. P. Wilkinson, "Nonlinear resonant circuit devices," U.S. Patent 3 624 125, July 16, 2018.
- [10] Caiquanwen and Z. Yang, "Electromagnetic field simulation of large hollow reactor," IOP Conference Series: Earth and Environmental Science, 512(1), 2020, pp. 1-11.